# Section 3.9 Experiments with Quantitative Factors, Goodness of Fit

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3.9 Experiments with Quantitative Factors, Goodness of Fit (Dose Response Modeling)

Example — Resin Glue Failure Time — Background

- How to measure the lifetime of things like computer disk drives, light bulbs, and glue bonds?
   E.g., a computer drive is claimed to have a lifetime of 800,000 hours (> 90 years).
   Clearly the manufacturer did not have disks on test for 90 years; how do they make such claims?
- Accelerated life test: Parts under stress (higher load, higher temperature, etc.) will usually fail sooner than parts that are unstressed. By modeling the lifetimes of parts under various stresses, we can estimate (extrapolate to) the lifetime of parts that are unstressed.
- Example: resin glue failure time

## Example — Resin Glue Failure Time<sup>1</sup>

- Goal: to estimate the life time (in hours) of an encapsulating resin for gold-aluminum bonds in integrated circuits (operating at 120°C)
- Method: accelerated life test
- Design: Randomly assign 37 units to one of 5 different temperature stresses (in Celsius)

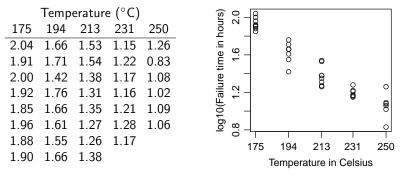
 $175^{\circ}, 194^{\circ}, 213^{\circ}, 231^{\circ}, 250^{\circ}$ 

- Treatments: temperature in Celsius
- Response: Y = log<sub>10</sub>(time to failure in hours) of the tested material.

<sup>&</sup>lt;sup>1</sup>Source: p. 448-449, *Accelerated Testing* (Nelson 2004). Original data is provided by Dr. Muhib Khan of AMD.

Example — Resin Glue Failure Time — Data

 $Y = \log_{10}(\text{Failure time in hours})$ 



Data file: resin.txt

Example — Resin Glue Failure Time — SS<sub>trt</sub>

Temperature (°C)	175	194	213	231	250
Size n <sub>i</sub>	8	8	8	7	6
Mean <u>y</u> i∙	1.9325	1.62875	1.3775	1.1943	1.0567
SD s <sub>i</sub>	0.0634	0.1048	0.1071	0.0458	0.1384

$$\overline{y}_{\bullet\bullet} = \frac{\sum n_i \overline{y}_{i\bullet}}{N}$$
  
=  $\frac{1}{37} (8 \cdot 1.9325 + 8 \cdot 1.62875 + 8 \cdot 1.3775 + 7 \cdot 1.1943 + 6 \cdot 1.0567)$   
\approx 1.4651

$$SS_{Trt} = \sum_{i=1}^{g} \sum_{j=1}^{n_i} (\overline{y}_{i\bullet} - \overline{y}_{\bullet\bullet})^2 = \sum_{i=1}^{5} n_i (\overline{y}_{i\bullet} - \overline{y}_{\bullet\bullet})^2$$
  
= 8(1.9325 - 1.4651)<sup>2</sup> + 8(1.62875 - 1.4651)<sup>2</sup> + 8(1.3775 - 1.4651)<sup>2</sup>  
+ 7(1.1943 - 1.4651)<sup>2</sup> + 6(1.0567 - 1.4651)<sup>2</sup>  
 $\approx 3.543$ 

## Example: Resin Glue Failure Time — SSE, F, and P-value

Temperature (°C)	175	194	213	231	250
Size n <sub>i</sub>	8	8	8	7	6
Mean <i>y</i> <sub>i∙</sub>	1.9325	1.62875	1.3775	1.1943	1.0567
SD s <sub>i</sub>	0.0634	0.1048	0.1071	0.0458	0.1384

$$SSE = \sum_{i=1}^{g} \sum_{j=1}^{n_i} (y_{ij} - \overline{y}_{i\bullet})^2 = \sum_{i=1}^{g} (n_i - 1) s_i^2$$
  
=  $(8 - 1)(0.0634)^2 + (8 - 1)(0.1048)^2 + (8 - 1)(0.1071)^2$   
+  $(7 - 1)(0.0458)^2 + (6 - 1)(0.1384)^2$   
 $\approx 0.2937$ 

$$F\text{-statistic} = \frac{SS_{Trt}/(g-1)}{SSE/(N-g)} = \frac{3.543/(5-1)}{0.2937/(37-5)} \approx 96.52$$

with g - 1 = 5 - 1 = 4 and N - g = 37 - 5 = 32 degrees of freedom.

The P-value is  $\approx 2.189\times 10^{-17}.$  The data exhibit strong evidence against the  $H_0$  that all means are equal.

```
> pf(96.52, df1 = 4, df2 = 32, lower.tail=F)
[1] 2.188913e-17
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```

## Always Check Degrees of Freedom

Something wrong? d.f. for tempC should be 5 - 1 = 4, not 1.

## Always Check Degrees of Freedom

As tempC is numerical, by default, R will fit the regression model

$$y_{ij} = \beta_0 + \beta_1 \texttt{tempC}_i + \varepsilon_{ij}.$$

rather than the ANOVA means model  $y_{ij} = \mu_i + \varepsilon_{ij}$ . We can let R treat tempC as *categorical* by as.factor()ing it.

### Means Model Is a Multiple Linear Regression Model

For an experiment with g treatments, the Means model

$$y_{ij} = \mu_i + \varepsilon_{ij}$$

can be written as a multiple linear regression model by defining a *dummy variable* for each treatment group. The dummy variable for the *i*th treatment is defined as

 $D_i = \begin{cases} 1 & \text{if the experimental unit receives the } i \text{th treatment} \\ 0 & \text{otherwise} \end{cases}$ 

The means model can then be written as a regression model

$$Y_k = \mu_1 D_{1k} + \mu_2 D_{2k} + \dots + \mu_g D_{gk} + \varepsilon_k$$

Note that this regression model has *no intercept*.

In R, putting -1 in the model formula tells R to fit a regression model with no intercept.

Recall for the resin glue data, the group means  $\overline{y}_{i\bullet}$  are

The command as.factor(tempC) tells R to create *dummy variables* for each levels the temperature. Without as.factor(), R will fit the model

$$y_{ij} = \beta t_i + \varepsilon_{ij}$$

where  $t_i$  is the temperature in Celsius for treatment group *i*.

```
> lmmeans1 = lm(y ~ -1 + tempC, data = resin)
> lmmeans1
Call:
lm(formula = y ~ -1 + tempC, data = resin)
Coefficients:
   tempC
0.006695
```

### If an Intercept Is Included in the Means Model...

The textbook formulate the means model in another form:

$$egin{aligned} & \mathbf{y}_{ij} = \mu_i + arepsilon_{ij} & ( ext{means model}) \ & = \mu + lpha_i + arepsilon_{ij} & ( ext{effects model}) \end{aligned}$$

- ► Observe the effects model has g + 1 parameters μ, α<sub>1</sub>,..., α<sub>g</sub>, while the means model only has g parameters μ<sub>1</sub>,..., μ<sub>g</sub>
- The effects model is overparameterized, meaning that it specifies more parameters than we actually need. The two sets of parameters below

$$(\mu, \alpha_1, \dots, \alpha_g)$$
 and  $(\mu - c, \alpha_1 + c, \dots, \alpha_g + c)$ 

specifies identical means for the responses. Thus the parameters for the effects model **cannot be uniquely determined**.

These two models are equivalent in the sense that fitted values for responses will be identical.

## When One of the $\alpha_i$ 's is Dropped ...

Say  $\alpha_1$  is dropped, the mean response for the g treatments are

$$\mathbb{E}[y_{ij}] = \begin{cases} \mu & \text{for treatment 1} \\ \mu + \alpha_2 & \text{for treatment 2} \\ \vdots & \\ \mu + \alpha_g & \text{for treatment g} \end{cases}$$

- The mean response under the first treatment (i = 1) is  $\mu$
- *α<sub>i</sub>* = the difference between the mean response of the *i*th treatment and that of the 1st treatment. One can compare the effect of the *i*th treatment and the 1st treatment by testing *α<sub>i</sub>* = 0
- Useful for comparing treatments

```
> lmeffects1 = lm(y ~ as.factor(tempC), data = resin)
> lmeffects1
```

```
Call:
lm(formula = y ~ as.factor(tempC), data = resin)
Coefficients:
(Iterret) = forter(terreC)104 = forter(t
```

(Intercept) as.factor(tempC)194 as.factor(tempC)213 1.9325 -0.3037 -0.5550 as.factor(tempC)231 as.factor(tempC)250 -0.7382 -0.8758

Note there is no as.factor(temp)175,  $\hat{\alpha}_1$ , since R sets  $\alpha_1 = 0$ .

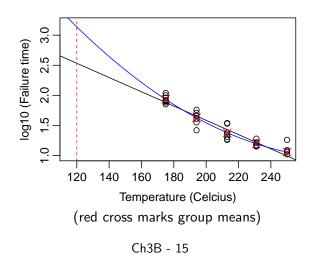
Temperature (°C)	175	194	213	231	250
$\overline{y}_{i\bullet}$	1.933	1.629	1.378	1.194	1.057

Observed  $\widehat{\mu} = \overline{y}_{1\bullet}$  and  $\widehat{\alpha}_i = \overline{y}_{i\bullet} - \overline{y}_{1\bullet}$ .

### Limitation of ANOVA F-Tests

The ANOVA *F*-test merely tells us the glue has different failure time at different temperature.

However, our goal is to predict the lifetime of the glue at a temperature of  $120^\circ.$ 



### Dose-Response Modeling

In some experiments, the treatments are associated with *numerical levels*  $x_i$  such as drug dose, baking time, or temperature.

We will refer to such levels as *doses*.

- ► The means model y<sub>ij</sub> = µ<sub>i</sub> + ε<sub>ij</sub> specifies **no relationship** between treatment levels x<sub>i</sub> and the response y, which cannot be used to infer the response at some dose x other than those used in the experiment
- With a *quantitative* treatment factor, experimenters are usually more interested on how the response is affected by the factor as a function of x<sub>i</sub>

$$y_{ij}=f(x_i;\theta)+\varepsilon_{ij},$$

e.g.,

$$f(x_i; \beta_0, \beta_1) = \beta_0 + \beta_1 x_i;$$
  

$$f(x_i; \beta_0, \beta_1, \beta_2) = \beta_0 + \beta_1 x_i + \beta_2 x_i^2; \text{ or }$$
  

$$f(x_i; \beta_0, \beta_1) = \beta_0 + \beta_1 \log(x_i).$$
  
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$$y_{ij} = f(x_i; \theta) + \varepsilon_{ij}$$

Advantages of dose-response modeling

- less complex (fewer parameters)
- easier to interpret (sometimes)

generalizable to doses not included in the experiment Issues to consider:

- ▶ How to choose the function *f*?
  - One commonly used family of functions *f* are *polynomials*:

$$f(x_i;\beta) = \beta_0 + \beta_1 x_i + \beta_2 x_i^2 + \cdots + \beta_k x_i^k,$$

But polynomials are NOT always the best choice

- For simplicity, we would choose the <u>lowest</u> possible order of polynomial that adequately fit the data.
- ▶ How to assess how well *f* fits the data? ...... Goodness of fit

## **Polynomial Models**

Let  $t_i$  denote the temperature in Celsius in treatment group *i*. Consider the following polynomial models for the resin glue data.

Null model :  $y_{ij} = \mu + \varepsilon_{ij}$ Linear model :  $y_{ij} = \beta_0 + \beta_1 t_i + \varepsilon_{ij}$ 2nd order model :  $y_{ij} = \beta_0 + \beta_1 t_i + \beta_2 t_i^2 + \varepsilon_{ij}$ 3rd order model :  $y_{ij} = \beta_0 + \beta_1 t_i + \beta_2 t_i^2 + \beta_3 t_i^3 + \varepsilon_{ij}$ 4th order model :  $y_{ij} = \beta_0 + \beta_1 t_i + \beta_2 t_i^2 + \beta_3 t_i^3 + \beta_4 t_i^4 + \varepsilon_{ij}$ 

- Every model is nested in the model below it. (Why?)
- Never skip a term. If a higher order term is significant, e.g.,  $t_i^3$ , than all lower order terms have to be kept  $(1, t_i, t_i^2)$ , even if they are not significant.
- Why not consider 5th order or higher order models?

In general, for an experiment with g treatment groups, if the treatment factor is numeric, one can fit a polynomial model up to degree g - 1

$$y_{ij} = \beta_0 + \beta_1 x_i + \dots + \beta_{g-1} x_i^{g-1} + \varepsilon_{ij}.$$

**Question**: For the resin glue data, what will happen if a quintic model (a polynomial of order 5) is fitted?

$$y_{ij} = \beta_0 + \beta_1 t_i + \beta_2 t_i^2 + \beta_3 t_i^3 + \beta_4 t_i^4 + \beta_5 t_i^5 + \varepsilon_{ij}$$

**Answer**: There exist <u>more than one</u> polynomial of degree 5 passing through the 5 points  $(175, \mu_1)$ ,  $(194, \mu_2)$ ,  $(213, \mu_3)$ ,  $(231, \mu_4)$ , and  $(250, \mu_5)$ . Thus the 6 coefficients  $\beta_0, \beta_1, \ldots, \beta_5$  CANNOT be uniquely determined.

As a rule of thumb, for an experiment with g treatments, we can fit a model with at most g parameters.

# Linear Model (1)

Let's try fitting the linear model:  $y_{ij} = \beta_0 + \beta_1 t_i + \varepsilon_{ij}$ .

- Fitted equation:  $\log_{10}(\text{failure time}) = 3.956 0.01186T$
- Predicted log<sub>10</sub>(failure time) at 120° is

 $3.956 - 0.01186 \times 120 \approx 2.5332$ ,

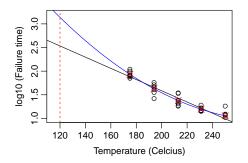
and hence the failure time at  $120^\circ$  is predicted as

 $10^{2.5332} \approx 341$  hours.

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# Linear Model (2)

R commands for the predicted log10(failure time) along with a 95% prediction interval:



By imposing the regression line on the top of the scatter plot, we can see y is a slightly curved with temperature. Using the linear model, the failure time at 120° will be *underestimated*.

### 2nd Order Model

- Fitted model:  $\log_{10}(\text{time}) = 7.418 0.0451T + 0.0000786T^2$
- Predicted log10(time) at 120° is

 $7.418 - 0.0451 \times 120 + 0.0000786 \times (120)^2 \approx 3.138$ 

The predicted failure time at  $120^{\circ}$  is  $10^{3.138} \approx 1374$  hours.

#### 3rd and 4th Order Models

> lm3 = lm(y ~ tempC+I(tempC^2)+I(tempC^3), data = resin)
> summary(lm3)

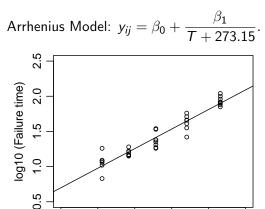
	Estimate	Std. Error	t value	Pr(> t )
(Intercept)	6.827e+00	1.299e+01	0.526	0.603
tempC	-3.659e-02	1.865e-01	-0.196	0.846
I(tempC^2)	3.815e-05	8.860e-04	0.043	0.966
I(tempC^3)	6.357e-08	1.392e-06	0.046	0.964

> lm4 = lm(y ~ tempC+I(tempC^2)+I(tempC^3)+I(tempC^4), data = resin)
Coefficients:

	Estimate	Std. Error	t value	Pr(> t )
(Intercept)	9.699e-01	1.957e+02	0.005	0.996
tempC	7.573e-02	3.750e+00	0.020	0.984
I(tempC^2)	-7.649e-04	2.679e-02	-0.029	0.977
I(tempC^3)	2.600e-06	8.459e-05	0.031	0.976
I(tempC^4)	-2.988e-09	9.962e-08	-0.030	0.976

### Arrhenius Law

The Arrhenius rate law in Thermodynamics says, the log of failure time is linear in the inverse of absolute Kelvin temperature, which equals the Centigrade temperature plus 273.16 degrees.



1/(Centigrate Temperature +273.15)

0.0020

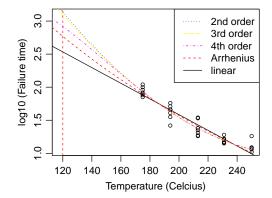
0.0022

0.0018

> lmarr = lm(y ~ I(1/(tempC+273.15)), data=resin)

> summary(lmarr)





Predicted log<sub>10</sub>(failure time) at 120° is  $-4.312 + \frac{2783.78}{120+273.15} \approx 2.77$ . The predicted failure time is  $e^{2.77} \approx 588$  hours.

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### Data Can Distinguish Models Only at Design Points

In addition to polynomial models and the Arrhenius model, many other models can be considered

$$y_{ij} = \beta_0 + \beta_1 \log(t_i) + \varepsilon_{ij},$$
  

$$y_{ij} = \beta_0 + \beta_1 \exp(t_i) + \varepsilon_{ij},$$
  

$$y_{ij} = \beta_0 + \beta_1 \sin(t_i) + \varepsilon_{ij},$$
  

$$y_{ij} = \beta_0 + f(t_i) + \varepsilon_{ij}.$$

As we only have observations at five temperatures:

175, 194, 213, 231, 250,

the data cannot distinguish between two models:

$$y_{ij} = f(t_i) + \varepsilon_{ij}$$
 and  $y_{ij} = g(t_i) + \varepsilon_{ij}$ ,

if f(t) and g(t) coincide at t = 175, 194, 213, 231, 250, even if f and g behave differently in other places.

### The Model that Fit the Data the Best

If no restriction is placed on f, how well the model  $y_{ij} = f(t_i) + \varepsilon_{ij}$  can possibly fit the data?

The least square method will choose the f that minimize

$$\sum_{i}\sum_{j}(y_{ij}-f(t_i))^2$$

Recall that given a list of numbers  $x_1, x_2, \ldots, x_n$  the *c* that minimize  $\sum_{i=1}^{n} (x_i - c)^2$  is the mean  $\overline{x} = \frac{1}{n} \sum_{i=1}^{n} x_i$ . Thus the least square method will choose the *f* that

$$f(t_i)=\overline{y}_{i\bullet}.$$

Thus the smallest SSE a model  $y_{ij} = f(t_i) + \varepsilon_{ij}$  can possibly achieve is

$$\sum_{i}\sum_{j}(y_{ij}-\overline{y}_{i\bullet})^2$$

which is the SSE for the **means model**  $y_{ij} = \mu_i + \varepsilon_{ij}$ .

Conclusion: no other models can beat the means model in minimizing the SSE. Ch3B - 27

### Goodness of Fit

As the means model is the model that fit the data the best, we can access the goodness of a model  $y_{ij} = f(t_i) + \varepsilon_{ij}$  by comparing it with the means model.

Full Model : 
$$y_{ij} = \mu_i + \varepsilon_{ij}$$
  
Reduced Model :  $y_{ij} = f(t_i) + \varepsilon_{ij}$ 

This comparison is legitimate because any model  $y_{ij} = f(t_i) + \varepsilon_{ij}$  is nested in the means model  $y_{ij} = \mu_i + \varepsilon_{ij}$  (letting  $\mu_i = f(t_i)$ ).

We can use the F-statistic below to compare a reduced model with a full model

$$F = \frac{(SSE_{reduced} - SSE_{full})/(df_{reduced} - df_{full})}{SSE_{full}/df_{full}}$$

### Goodness of Fit of the Linear Model

Since the linear model (reduced model) is nested in the means model (full), use the *F*-statistic for model comparison we get

```
2 32 0.29369 3 0.07837 2.8463 0.05303 .
```

The P-value 0.05303 is moderate evidence showing the linear doesn't fit the data so well.

### Goodness of Fit of the 2nd-Order Model

Since the 2nd-order model (reduced model) is also nested in the means model (full model), again using the *F*-statistic for model comparison we get

```
> lm2 = lm(y ~ tempC+I((tempC)^2), data=resin)  # 2nd-order model
> lmmeans = lm(y ~ as.factor(tempC), data = resin)  # means model
> anova(lm2,lmmeans)
Analysis of Variance Table
Model 1: y ~ tempC + I((tempC)^2)
Model 2: y ~ as.factor(tempC)
  Res.Df  RSS Df  Sum of Sq   F Pr(>F)
1     34 0.29372
2     32 0.29369  2 2.6829e-05 0.0015 0.9985
```

The large *p*-value 0.9985 shows the 2nd-order model fits the data nearly as good as the best model. Does this indicate the 2nd-order model is an adequate model?

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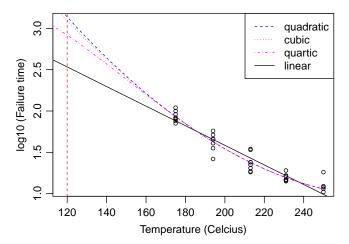
Shall We Consider a 3rd- or 4th-Order Model?

No. Because

 $2\mathsf{nd}\text{-}\mathsf{order} \subset 3\mathsf{rd}\text{-}\mathsf{order} \subset 4\mathsf{th}\text{-}\mathsf{order} \subset \mathsf{Means}\ \mathsf{Model}$ 

the 3rd- or 4th-order model won't fit the data better than the means model does. As the 2nd-order model fits the data nearly as well as the means model, the 4 models just fit as well as each other. In this case we simply choose the model of lowest complexity.

#### Be Cautious About Extrapolation



Though the 2nd-, 3rd-, 4th-order model fit the 5 points nearly as well, their predicted values at 120°C are quite different,

2nd-order > 3rd-order > 4th-order > linear Ch3B - 32 Since the Arrhenius model is nested in the means model, we can check its goodness of fit.

The moderately large *P*-value 0.2749 told us the Arrhenius Model is acceptable relative to the best model.